

An Estimation-Based Approach to the Design of Adaptive IIR Filters ¹

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Abstract

We present an estimation-based approach to the design of adaptive IIR filters. We also use this approach to design adaptive filters when a feedback signal from the output of the adaptive filter contaminates the reference signal. We use an H_∞ criterion to cast the problem as a nonlinear H_∞ filtering problem, and present an approximate linear H_∞ filtering solution. This linear filtering solution is then used to adapt the adaptive IIR Filter. The presentation of the proposed adaptive algorithm is done in the context of an adaptive Active Noise Cancellation (ANC) problem. Simulations are used to examine the performance of the proposed estimation-based adaptive algorithm.

1 Introduction

The Least-Mean Squares (LMS) adaptive algorithm [1] has been used for over 35 years as the center piece of a wide variety of adaptive algorithms. Despite numerous successful applications, it was only recently that the H_∞ optimality of the LMS algorithm was established [2], and its important properties, such as bounds on adaptation rates, were rigorously derived.

Over years, however, numerous (mostly heuristic) variations of the LMS algorithm have been developed to overcome practical implementation problems (see [1] and [4] for instance). The contamination of the reference signal (see Figure 1) with the output of the adaptive filter has proven to further complicate the implementation problems. Thus systematic approaches for the design and analysis of the adaptive filters for realistic control scenarios have been of primary interest to researchers in the field. In [3], an estimation-based approach to the design of adaptive FIR filters is proposed. Reference [3] uses an adaptive ANC scenario to explain how an estimation interpretation of the adaptive control problem provides a framework for the systematic synthesis and analysis of adaptive FIR filters. This paper extends the results in [3] to the design of adaptive Infinite Impulse Response (IIR) filters. The formulation presented here also applies when the reference signal is contaminated with a feedback from the output of the adaptive filter (Figure 1).

The effects of the reference signal contamination has been studied in the adaptive control literature (see Chapter 3 of [4] and the references therein). *Feedback neutralization*

is one approach which uses a separate feedback within the adaptive controller to cancel the effect of the undesired feedback [6]. This scheme, however, requires special care in the implementation to avoid the cancellation of the reference signal all together (see [4] for details). Looking at feedback neutralization from a different point of view, it is clear that this algorithm generates poles as well as zeros for the overall adaptive filter. In other words, the overall adaptive controller is an IIR filter in general (and hence stability of the overall system should be closely monitored). Observing this fact, there have been several attempts to directly design an adaptive IIR filter in such circumstances. Filtered-U recursive LMS algorithm is one such approach. In this technique, the feedback path is explicitly treated as part of the plant, [7], and the derivation involves approximations that rely on slow adaptation. Furthermore, there are many concerns about the convergence properties of this scheme [4]. It is also noted that the optimal solution can be extremely ill-conditioned if a large number of controller coefficients are used or the structure of feedback path is complicated.

This paper's estimation-based approach to the design of adaptive IIR filters, in essence meets a disturbance attenuation criterion (to be defined shortly), and hence provides a framework in which the questions about convergence and stability of the adaptive algorithm can be systematically addressed. Moreover, the estimation-based approach easily extends to the case where the reference signal available to the adaptive algorithm is contaminated with the feedback from the output of the adaptive filter.

This paper is organized as follows. Section 2 presents the estimation-based formulation for the adaptive filter design. Section 3 discusses the H_∞ -optimal solution to the formulated estimation problem. Section 4 outlines our proposed implementation scheme for the adaptive algorithm. Section 5 contains simulation results. Section 6 concludes this paper with a summary and final remarks.

2 Problem Formulation

We discuss the estimation-based approach to the design of an adaptive IIR filter (with and without the presence of a feedback path) in the context of the ANC problem of Figure 1. In this section we first concentrate on the case where there is no feedback path. The case with feedback path is then an straightforward extension.

The objective of ANC is to generate a control signal $u(k)$ such that the output of the secondary path, $y(k)$, is in some measure (to be specified later) close enough to the output of the primary path, $d(k)$. For this to materialize, the series connection of the IIR filter (for some optimal setting of its parameters) and the known secondary path must appropriately approximate the unknown pri-

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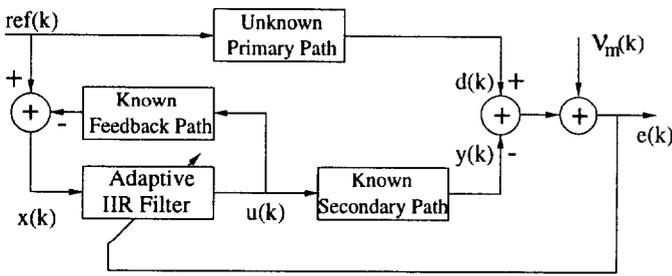


Fig. 1: Block Diagram of an ANC Problem With Feedback Contamination of the Reference Signal

primary path. Figure 2 captures this notion. This observation, in our view, is an *estimation interpretation* of the adaptive control problem. Note that as long as the output of the “modeling error” block in Figure 2 is bounded, then it can be treated as a component of the measurement disturbance signal, $\mathcal{V}_m(k)$.

To formalize this observation, we assume a state space model for the IIR filter and the secondary path, and then form an approximate model for the primary path as shown in Figure 3. This approximate model is the closest to the actual primary path for some optimal (but unknown) setting of the filter parameters. Now, the estimation-based approach to the design of an adaptive IIR filter is described as follows:

1. Devise an estimation strategy that recursively improves our estimate of the optimal values of the IIR filter parameters in the approximate model of the primary path (given the available measurement history to be described shortly),
2. Set the actual value of the parameters in the adaptive IIR filter to the best estimate of the parameters obtained from the estimation strategy.

We now take a closer look at the main signals in Figure 2. Note that $e(k) = d(k) - y(k) + \mathcal{V}_m(k)$, where

- a) $e(k)$ is the available error measurement,
- b) $\mathcal{V}_m(k)$ is the exogenous disturbance that captures measurement noise, modeling error and initial condition uncertainty for the secondary path,
- c) $y(k)$ is a known signal, because (i) $u(k)$ is exactly known (we directly set the parameters in the IIR filter), and (ii) we assume that θ_0 (the initial condition for the secondary path) is known¹.

The *derived* measured quantity, $m(k)$ in Figure 3, can now be defined as

$$m(k) \triangleq e(k) + y(k) = d(k) + \mathcal{V}_m(k) \quad (1)$$

2.1 Estimation Problem

Figure 3 reflects a block diagram representation of the approximate model to the primary path. We assume a

¹Note that as long as the effect of the initial condition in the output of the secondary path does not grow without bound, any error in $y(k)$ (due to an initial condition other than what we assumed) can be treated as a component of the measurement disturbance.

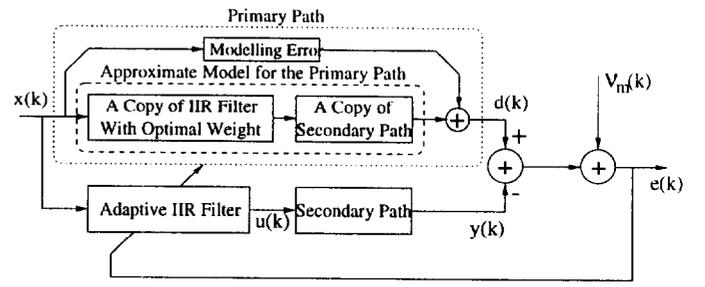


Fig. 2: Estimation Interpretation of the IIR Adaptive Filter Design in a ANC Problem

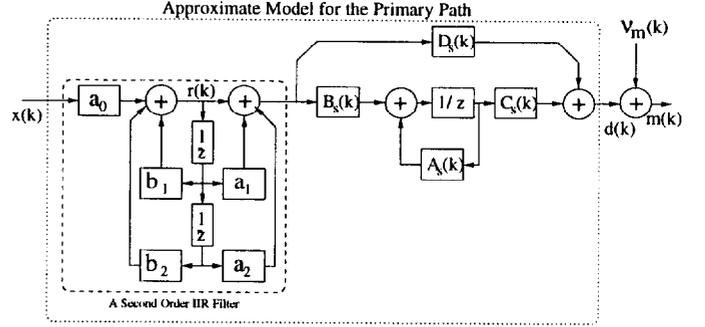


Fig. 3: Approximate Model For the Unknown Primary Path (A second order IIR filter is shown here)

state space model, $[A_s(k), B_s(k), C_s(k), D_s(k)]$, for the replica of the secondary path in Figure 3. We also define $W(k) = [a_0(k) \ b_1(k) \ \dots \ b_N(k) \ a_1(k) \ \dots \ a_N(k)]^T$ to be the unknown optimal vector of the IIR filter parameters at time k . $\xi_k^T = [W(k)^T \ \theta(k)^T]$ is then the state vector for the overall system. Note that $\theta(k)$ captures the dynamics of the replica of the secondary path. The state space representation of the system is then

$$\underbrace{\xi^{(k+1)}}_{\begin{bmatrix} W(k+1) \\ \theta(k+1) \end{bmatrix}} = \underbrace{F_k}_{\begin{bmatrix} I_{(2N+1) \times (2N+1)} & 0 \\ B_s(k)h_k^* & A_s(k) \end{bmatrix}} \underbrace{\xi^{(k)}}_{\begin{bmatrix} W(k) \\ \theta(k) \end{bmatrix}} \quad (2)$$

where

$$h_k = [x(k) \ r(k-1) \ \dots \ r(k-N) \ r(k-1) \ \dots \ r(k-N)]^T$$

captures the effect of the reference input $x(\cdot)$. Note that

$$r(k) = x(k)a_0(k) + r(k-1)b_1(k) + \dots + r(k-N)b_N(k),$$

$$r(-1) = \dots = r(-N) = 0 \quad (3)$$

and therefore, the system dynamics are *nonlinear* in the IIR filter parameters. For this system, the *derived* measured output is

$$m(k) = \underbrace{H_k}_{\begin{bmatrix} D_s(k)h_k^* & C_s(k) \end{bmatrix}} \underbrace{\xi^{(k)}}_{\begin{bmatrix} W(k) \\ \theta(k) \end{bmatrix}} + \mathcal{V}_m(k) \quad (4)$$

where $m(k)$ should be constructed at each step according to Equation (1). Once again, the measurement equation is also nonlinear in the parameters of the IIR filter. Now, define a generic linear combination of the states as the

desired quantity to be estimated

$$s(k) = \overbrace{\begin{bmatrix} L_{1,k} & L_{2,k} \end{bmatrix}}^{L_k} \begin{bmatrix} W(k) \\ \theta(k) \end{bmatrix} \quad (5)$$

Note that $m(\cdot) \in \mathcal{R}^{p \times 1}$, $s(\cdot) \in \mathcal{R}^{q \times 1}$, $\theta(\cdot) \in \mathcal{R}^{r \times 1}$, and $W(\cdot) \in \mathcal{R}^{(2N+1) \times 1}$. All matrices are then of appropriate dimensions.

To allow for a simplified solution (see Section 3), of all choices available for L_K , $L_K = H_k$ is considered here. In principle, any estimation algorithm can now be used to generate $\hat{s}(k|k) \triangleq \mathcal{F}(m(0), \dots, m(k))$ (a causal estimate of the desired quantity, $s(k)$) such that some *closeness* criterion is met. This paper focuses on an H_∞ estimation criterion. Here, the main objective is to limit the worst case energy gain from the measurement disturbance and the initial condition uncertainty to the error in a causal estimate of $s(k)$. In other words, it is desired to find an H_∞ suboptimal causal estimator $\hat{s}(k|k) = \mathcal{F}(m(0), \dots, m(k))$ such that

$$\sup_{\mathcal{V}_m, \xi_0} \frac{\sum_{k=0}^M [s(k) - \hat{s}(k|k)]^* [s(k) - \hat{s}(k|k)]}{\xi_0^* \Pi_0^{-1} \xi_0 + \sum_{k=0}^M \mathcal{V}_m^*(k) \mathcal{V}_m(k)} \leq \gamma^2 \quad (6)$$

Note that, in this case

1. There is no statistical assumption regarding the measurement disturbance. Therefore, the error in the modeling of the primary path can be easily treated as a component of the measurement disturbance. For large modeling error, however, the performance can be expected to deteriorate.
2. A closed form solution to the nonlinear H_∞ estimation problem is not available. To derive a recursion for the filter parameter update, we apply the following approximation: *At each time step, replace the IIR filter parameters in Equation (3) with their best available estimate.* This reduces the problem into a linear H_∞ estimation problem for which a solution similar to that in [3] exists².

3 H_∞ -Optimal Solution

In this section, we only quote the γ -suboptimal filtering solution for the *linearized* H_∞ -estimation problem [5,8]. The arguments for the optimal value of γ for the solution to the linearized problem and the simplifications that follows are similar to those presented in [3] and hence are not repeated here.

²As Figure 3 suggests, *feedback* is an integral part of an IIR filter structure. The discussion in Section 2.1 showed that this feedback results in the nonlinearity in the system dynamics. The same holds true when a feedback path exists such that the reference signal is contaminated by the output of the adaptive filter itself (Figure 1). Our treatment of the nonlinearity in the case of an IIR filter, i.e. replacing the IIR filter parameters in Equation (3) with their best available estimates, carries over to the case where such a feedback path exists.

3.1 γ -Suboptimal Finite Horizon Filtering Solution

Theorem [5]: Consider the system in Figure 3 and described by Equations (2)-(5). Assume that the linearizing approximation discussed in the previous section is applied. A level- γ H_∞ filter that achieves (6) exists if, and only if, the matrices R_k and $R_{e,k}$ defined by

$$R_{e,k} = \overbrace{\begin{bmatrix} I_p & 0 \\ 0 & -\gamma^2 I_q \end{bmatrix}}^{R_k} + \begin{bmatrix} H_k \\ L_k \end{bmatrix} P_k \begin{bmatrix} H_k^* & L_k^* \end{bmatrix} \quad (7)$$

have the same inertia for all $0 \leq k \leq M$, where $P_0 = \Pi_0$ and $P_k > 0$ satisfies the Riccati recursion

$$P_{k+1} = F_k P_k F_k^* - K_{p,k} R_{e,k} K_{p,k}^* \quad (8)$$

where $K_{p,k} = (F_k P_k \begin{bmatrix} H_k^* & L_k^* \end{bmatrix}) R_{e,k}^{-1}$. If this is the case, then the central H_∞ estimator is given by

$$\hat{\xi}_{k+1} = F_k \hat{\xi}_k + K_{1,k} (m(k) - H_k \hat{\xi}_k), \quad \hat{\xi}_0 = 0 \quad (9)$$

$$\hat{s}(k|k) = L_k \hat{\xi}_k + (L_k P_k H_k^*) R_{H_{e,k}}^{-1} (m(k) - H_k \hat{\xi}_k) \quad (10)$$

with $K_{1,k} = (F_k P_k H_k^*) R_{H_{e,k}}^{-1}$ and $R_{H_{e,k}} = I_p + H_k P_k H_k^*$. The optimal value of γ is 1 (see Refs. [2,3]), and for this optimal value the Riccati equation in (8) reduces to $P_{k+1} = F_k P_k F_k^*$.

3.2 Important Remarks

1. As in the case for the FIR filter design, the estimation-based approach to the design of the adaptive IIR filter requires the solution to only one Riccati equation. Furthermore, the Riccati solution propagates *forward* in time and does not involve any information regarding the future of the system or the reference signal. Thus, the resulting adaptive algorithm is real-time implementable.
2. As mentioned in Section 3.1, the Riccati update (for the simplified solution) reduces to a Lyapunov recursion which always generates a positive definite P_k as long as $P_0 > 0$. This eliminates the need for computationally expensive checks for positive definiteness of P_k at each step.
3. In general, the solution to an H_∞ filtering problem requires verification of the fact that R_k and $R_{e,k}$ are of the same inertia at each step. This can be a computationally expensive task. Our formulation of the problem eliminates the need for such checks by allowing a definitive answer to the feasibility of $\gamma = 1$. This also guarantees that a breakdown in the solution will not happen.
4. With no need to verify the solutions at each step, the computational complexity of the estimation based approach is $O(n^3)$ (in calculating $F_k P_k F_k^*$), where $n = 2N + 1$ (number of IIR filter Parameters) + $n_{sec-path}$ (the order of the secondary path). The special structure of F_k however reduces the computational complexity involved to $O(n_{sec-path}^3)$. This can be a substantial reduction in the computation when $2N + 1$ is large compared to $n_{sec-path}$.

4 Estimation-Based Adaptive Algorithm

In this section, we use three sets of variables to describe the adaptive algorithm, (i) $\hat{W}(k)$ and $\hat{\theta}(k)$ (best estimate

of the state at time k), (ii) $\theta_{actual}, u(k) \triangleq h_k^* \hat{W}(k), y(k)$, and $d(k)$ (the actual value of the variables), and (iii) adaptive algorithm's internal copy of a variable (referred to with subscript “*copy*”). See [3] for a detailed description of these variables. We outline the implementation algorithm as follows:

1. Start with $\hat{W}(0) = \hat{W}_0, \hat{\theta}(0) = \hat{\theta}_0$ as the best initial guess for the state vector in the approximate model of the primary path. Assume that the IIR filter starts with $r(-1) = \dots = r(-N) = 0$. Also consider $\theta_{actual}(0) = \theta_{actual,0}$, while the adaptive algorithm assumes that $\theta_{copy}(0) = \theta_{copy,0}$. Furthermore, $d(0)$ is the initial output of the primary path. Then, for $0 \leq k \leq M$ (*finite horizon*):

2. Form h_k (with the available estimate of the parameter vector $\hat{W}(k)$),

3. Form the control signal $u(k) = h_k^* \hat{W}(k)$,

4. Apply the control signal to the secondary path. The actual output and the new state vector have dynamics

$$\begin{aligned} \theta_{actual}(k+1) &= A_s(k)\theta_{actual}(k) + B_s(k)u(k) \\ y(k) &= C_s(k)\theta_{actual}(k) + D_s(k)u(k) \end{aligned} \quad (11)$$

5. Propagate the internal copy of the state vector and the output of the secondary path as

$$\begin{aligned} \theta_{copy}(k+1) &= A_s(k)\theta_{copy}(k) + B_s(k)u(k) \\ y_{copy}(k) &= C_s(k)\theta_{copy}(k) + D_s(k)u(k) \end{aligned} \quad (12)$$

6. Form the *derived* measurement, $m(k)$, using the direct measurement $e(k)$ and the copy of the output of the secondary path $m(k) = e(k) + y_{copy}(k)$. Note that $e(k)$ is the error measured after the control signal $u(k)$ is applied.

7. Use the H_∞ -optimal estimator's state update, Equations (9), to find the H_∞ -optimal estimate of the optimal IIR filter parameters in Figure 3 (i.e. $\hat{W}(k+1)$). Note that $\hat{\theta}(k+1)$ should also be stored for the next estimation update.

8. If $k \leq M$, go to 2.

The example in the following section indicates that this algorithm performs well. We are currently investigating the impact of the use of y_{copy} in this algorithm.

5 Simulation

This section examines the performance of the adaptive algorithm described in Section 4. For the simulations in this section, second order systems, $P(z) = \frac{z-0.3}{(z+0.4-j0.8)(z+0.4+j0.8)}$, and $S(z) = \frac{z-0.3}{(z+0.65-j0.7)(z+0.65+j0.7)}$, (with different damping ratios and resonance frequencies) are used as primary and secondary paths. The primary path is unknown to the adaptive algorithm. We use a second order adaptive IIR filter (and hence the parameter vector for the IIR filter is of length 5). We examine the performance of the adaptive IIR filter with and without feedback contamination. For the feedback path another second order system, $F(z) = \frac{z-0.3}{(z+0.2-j0.75)(z+0.2+j0.75)}$, is used. A multi-tone signal, $x(k) = \sum_{i=1}^3 10 \sin(2\pi f_i k \Delta t)$ (where $f_1 = 3.0, f_2 = 4.5$, and $f_3 = 15$ Hz), is used as the reference signal. As measurement noise, $\mathcal{V}_m(k)$, we

use a zero mean, normally distributed random variable with variance 0.01. Furthermore, $\Delta t = 0.01$ seconds and $P_0 = 0.05I$.

Figure 4 captures the performance of the adaptive IIR filter with the multi-tone reference signal described above when no feedback contamination exists. The error plot indicates an effective cancellation of the output of the primary path in roughly 1.5 seconds. Figure 5 clearly indicates that the existence of a feedback path from the output of the adaptive filter to the reference signal, results in a slower convergence of the adaptive IIR filter. Nevertheless, the adaptive filter successfully reduces the error in noise cancellation.

6 Conclusion

We have introduced a systematic, estimation-based approach to the design of adaptive IIR filters. This work extends our previous results in [3] (where an estimation-based approach to the design of FIR filters is introduced). We have also proposed an appropriate framework in which an IIR (as well as an FIR) filter can be designed when the reference signal is contaminated by a feedback from the output of the adaptive filter. The proposed algorithm uses an H_∞ filtering solution to limit the worst case energy gain from the measurement disturbance and initial condition uncertainty to the residual error energy. We have shown that this worst case energy gain is unity, and have exploited the structure of the formulation to simplify the filtering solution.

In our view, the proposed formulation in this paper provides an appropriate framework for robustness studies of adaptive filters. Furthermore, systematic optimization of the filter parameters (such as the order of the IIR filter) may be investigated.

Appendix A: Adaptive IIR Filter Design When Feedback Contamination Exists

Figure 6 reflects the block diagram for an approximate model of the primary path when a feedback path from the output of the IIR filter to its input exists. The derivation of an adaptive IIR filter in this case parallels that in Sections 2 and 3. Therefore, only the state space representation of this approximate model is outlined here:

$$\begin{bmatrix} \xi(k+1) \\ W(k+1) \\ \theta(k+1) \\ \varphi(k+1) \end{bmatrix} = \begin{bmatrix} I_{(2N+1) \times (2N+1)} & 0 & 0 \\ B_s(k)h_k^* & A_s(k) & 0 \\ B_f(k)h_k^* & 0 & A_f(k) \end{bmatrix} \begin{bmatrix} W(k) \\ \theta(k) \\ \varphi(k) \end{bmatrix}$$

where $\varphi(k)$ is the state vector for the feedback path, and h_k and $W(k)$ are the same as in Section 2.1. Note that

$$\begin{aligned} x(k) &= r e f(k) + D_f(k)h^*(k)W(k) + C_f(k)\varphi(k), \\ r(k) &= a_0 x(k) + b_1 r(k-1) + \dots + b_N r(k-N), \\ r(-1) &= \dots = r(-N) = 0 \end{aligned}$$

where the *contamination* of the reference signal with the feedback from the output of the adaptive filter is evident.

